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# TOWN OF DURHAM STORMWATER MANAGEMENT PLAN FOR CLARK PROPERTIES, LLC

# 74 MAIN STREET TAX MAP 106, LOT 59 (FORMERLY TAX MAP 2, LOT 14-1)

SUBMITTED ON 19 JULY 2021

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# **1. PROJECT INFORMATION NARRATIVE**

#### **1.1. Project narrative**

# 1.1.1. Project summary

Clark Properties, LLC intends to redevelop the property at 74 Main Street in Durham, New Hampshire (Tax Map 106, Lot 59). The project will demolish the existing 1100 ft<sup>2</sup> building on the property and construct five-story mixed-use building. Additionally, the parking and traffic flow will be modified. This report was prepared by Horizons Engineering to ensure the design of the stormwater management for 74 Main Street complies with the applicable federal, state and local regulations for stormwater.

# 1.1.2. Existing conditions

The proposed work is located at the corner of Main Street and Pettee Brook Lane. The project site currently consists of an office building and two paved parking areas with a combined 13 spaces. The stormwater runoff from the office building and the larger parking area in the north drain to catch basins on Pettee Brook Lane at the northeast side of the property. The stormwater runoff from the western portion of the site is collected in catch basins along Main Street. All the existing catch basins are part of Durham's municipal separate storm sewer system (MS4). The flow is split between two drainage points. The first point (PA-1) is located at a catch basin on Main Street. This catch basin is routed to the west into UNH property and ultimately outlets to College Brook. The second point (PA-2) is located at a catch basin on the northeast corner of the property along Pettee Brook Lane. The storm sewer ultimately outlets to the Pettee Brook.

# 1.1.3. Proposed site conditions & disturbances

In the proposed post-developed condition the majority of the lot will be covered by the new building. The majority of the remained of the land will be paved using pervious interlocking concrete pavers (PICP). A small remainder of the land, ca. 300 square feet will be grassed. Due to the negligible impact of this grassed area on the over runoff from the site, and the potential to compact the soils during construction, the entire lot has been modelled as impervious land cover.

The new building will have a roof area of about 6100 square feet. Two-thirds (4000 sq. ft.) of the roof will be routed to permeable paver system to infiltrate some of the runoff and buffer the peak flow. The remainder of the roof will be routed to a new catch basin (1P)

The permeable paver system have been split into three cells. The system is built on a max. 5% grade and two membrane barriers will be installed to create storage space on the slope. Overall the system takes up about 1880 sq. ft. with some of the open-graded reservoir stone extending below the concrete slab under the building overhang.

The runoff from the adjacent property (TM160, L61) will be collected along the property line. The design intent is to have a the concrete pad and concrete edge restraint to be 1/4" proud of the new asphalt to concentrate flow towards a new deep-sump catch basin (2P). The purpose of this to prevent heavily sediment laden runoff from flowing directly into the PICP system. It is expected that during larger storms, the flow depth in this location may exceed 1/2" for very short periods of time, and the PICIP is able to handle these additional flows without ponding.

The remainder of the runoff form the site are the narrow strip between the front of the building and the road which currently flows to the street, and a small 300 sq. ft. area by the proposed transformer pad. These areas will be collected in the existing catch basins located on Pettee Brook Lane (E2) and on the abutting town property (E1).

The flows towards PA-1 have been reduced due to the removal of the paved area on the abutting property.

# 1.1.4. Hydrologic data and methods

The stormwater model was built in the software program HydroCAD (Version 10.00 25). HydroCAD uses the methods described in the NRCS National Engineering Handbook [2] to create rainfall-runoff relationships, determine time of concentration, generate unit hydrographs for each subcatchment area.

The direct runoff from the site was estimated using the Weighted-Q method. Synthetic design storms used rainfall data and intensity curves from the NOAA (Atlas 14). Soils maps generated by the Natural Resources Conservation Service (NRCS), and land cover data from the field survey were used to determine the soil-complex CN values.

Using SCS TR-20, run under HydroCAD Version 10.0 with 24-hour rainfall events based on Atlas 14 data for Durham, NH, pre- and post-development cover types and drainage paths were modeled to generate peak discharge rates. These data are provided in full in section 1.3 of this report and are summarized below in Table 1.1.

Storm	Depth [inches]
1″	1.00
2-YR	3.30
10-YR	5.29
25-YR	6.53
50-YR	7.44
100-YR	8.44

Table 1.1: Project design storm depths from NOAA

# 1.1.5. Peak runoff control requirement

Town of Durham Site Design Standards require that measures be taken to control the post-development peak rate runoff so that it does not exceed pre-development runoff for the 1 inch, 2-, 10-, and 17<sup>1</sup>- year, 24-hour storm events. Due to the post-project grading of the site and changes in land cover, stormwater devices were used to attenuate flow in order to meet these Peak Runoff Control requirements. Table 1.2 summarizes the stormwater runoff peak flow rate for the 1 inch, 2-, 10- and 25-year storm events.

1					
Pe	Peak flow [ft2/s]				
	PA	-1	PA	-2	
Storm	Pre	Post	Pre	Post	
1″	0.28	0.22	0.19	0.19	
2-YR	1.07	0.93	0.83	0.77	
10-YR	1.71	1.53	1.40	1.13	
25-YR	2.12	1.95	1.76	1.41	
50-YR	2.43	2.25	2.03	1.62	
100-YR	2.75	2.57	2.32	1.80	

Table 1.2: Peak flow from 74 Main Street

The peak flows for all events are decreased in the post-development condition, except the 1" storm which is the same as the pre-development condition.

<sup>&</sup>lt;sup>1</sup> Understood to be a typo and the 25-year rainfall event is intended

#### 1.1.6. Infiltration volume requirement

A permeable interlocking concrete paver (PICP) systems was selected to store water, and allow for slow infiltration into the existing soils. The existing soils are estimated to have an infiltration rate of 0,5 in/hr. This rate is enough to allow for some infiltration but, in larger storms with long recurrence intervals (>10 year) it is not possible to prevent runoff through infiltration alone. The PICP system does allow more infiltration to the site than in the pre-existing conditions. Therefore, no additional calculations were done to determine if the minimum volume requirement was met. See section 1.1.7 for more information.

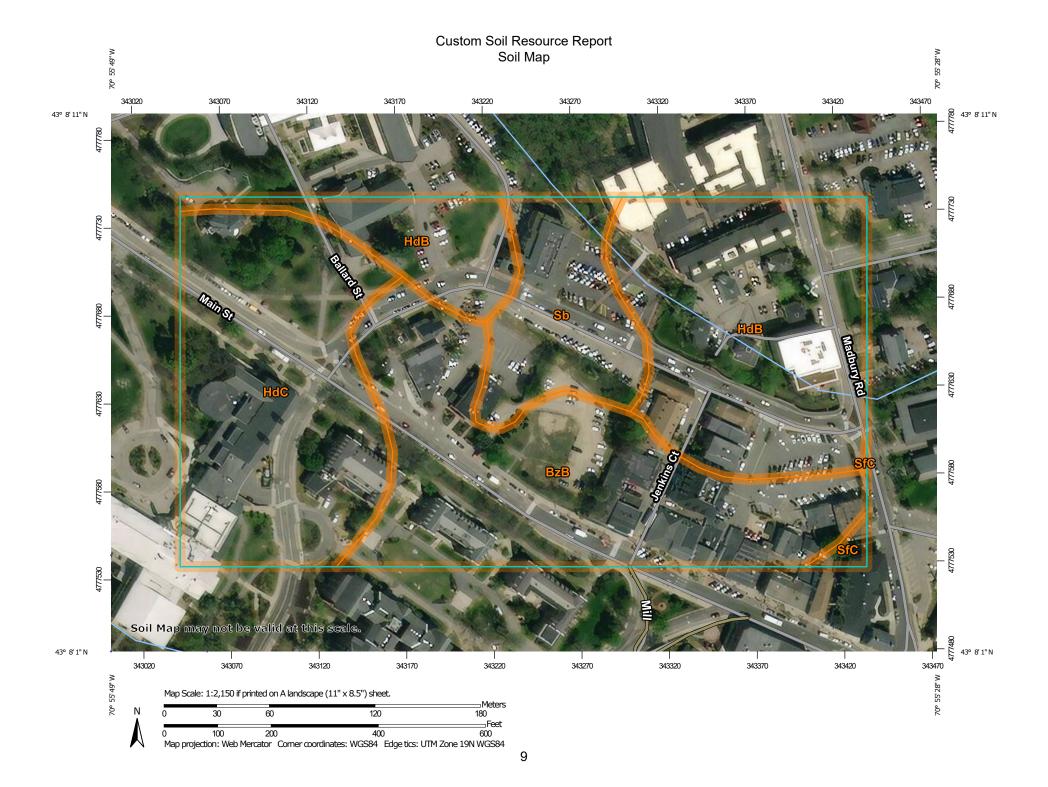
# 1.1.7. Runoff volume control

The runoff volume from each storm event is summarized in table 1.3.

Peak flow [ft3]				
	PA-	1	PA	-2
Storm	Pre	Post	Pre	Post
1″	834	678	591	547
2-YR	3532	3086	2747	2662
10-YR	6048	5433	4873	4766
25-YR	7649	6945	6247	6058
50-YR	8833	8069	7269	7048
100-YR	10 141	9314	8402	8208

*Table 1.3: 74 Main Street storm runoff volumes* 

In all events the volume of runoff leaving the site is less in the post-development conditions than the predevelopment conditions. 1.2. NRCS soils information



	MAP LEGEND			MAP INFORMATION
Area of In	iterest (AOI)	100	Spoil Area	The soil surveys that comprise your AOI were mapped at
	Area of Interest (AOI)	۵	Stony Spot	1:20,000.
Soils	Soil Map Unit Polygons	Ø	Very Stony Spot	Warning: Soil Map may not be valid at this scale.
	Soil Map Unit Lines	Ŷ	Wet Spot	
~	Soil Map Unit Points	$\triangle$	Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil
En acial	·		Special Line Features	line placement. The maps do not show the small areas of
Special (0)	Point Features Blowout	Water Fea	atures	contrasting soils that could have been shown at a more detailed scale.
×	Borrow Pit	$\sim$	Streams and Canals	
×	Clay Spot	Transport	tation Rails	Please rely on the bar scale on each map sheet for map measurements.
$\diamond$	Closed Depression	~	Interstate Highways	
X	Gravel Pit	~	US Routes	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
0 00	Gravelly Spot	Major Roads	Coordinate System: Web Mercator (EPSG:3857)	
0	Landfill	~	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator
٨.	Lava Flow	Backgrou	Ind	projection, which preserves direction and shape but distorts
علله	Marsh or swamp	and the second	Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more
衆	Mine or Quarry			accurate calculations of distance or area are required.
0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as
0	Perennial Water			of the version date(s) listed below.
$\vee$	Rock Outcrop			Soil Survey Area: Strafford County, New Hampshire
+	Saline Spot			Survey Area Data: Version 20, May 29, 2020
° °	Sandy Spot			Soil map units are labeled (as space allows) for map scales
=	Severely Eroded Spot			1:50,000 or larger.
\$	Sinkhole			Date(s) aerial images were photographed: Dec 31, 2009—Sep
≫	Slide or Slip			9, 2017
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
BzB	Buxton silt loam, 3 to 8 percent slopes	6.1	29.8%
HdB	Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes	6.6	32.4%
HdC	Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes	5.4	26.6%
Sb	Saugatuck loamy sand	2.2	10.6%
SfC	Suffield silt loam, 8 to 15 percent slopes	0.1	0.6%
Totals for Area of Interest		20.4	100.0%

# Map Unit Legend

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

# **Strafford County, New Hampshire**

# BzB—Buxton silt loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d6p Elevation: 0 to 260 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Buxton and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Buxton**

#### Setting

Parent material: Glaciomarine

#### **Typical profile**

H1 - 0 to 10 inches: silt loam H2 - 10 to 28 inches: silty clay loam H3 - 28 to 43 inches: silty clay

#### **Properties and qualities**

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 12 to 24 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C/D Ecological site: F145XY006CT - Semi-Rich Moist Lake Plain Hydric soil rating: No

#### **Minor Components**

#### Elmwood

Percent of map unit: 10 percent Hydric soil rating: No

#### Not named

*Percent of map unit:* 5 percent *Hydric soil rating:* No

# HdB—Hollis-Charlton very rocky fine sandy loams, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7m Elevation: 0 to 1,000 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 120 to 240 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Hollis and similar soils: 40 percent Charlton and similar soils: 30 percent Minor components: 30 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Hollis**

#### Setting

Parent material: Till

#### Typical profile

*H1 - 0 to 14 inches:* very stony fine sandy loam *H2 - 14 to 18 inches:* bedrock

#### **Properties and qualities**

Slope: 3 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 10 to 20 inches to lithic bedrock
Drainage class: Well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Parent material: Till

#### **Typical profile**

H1 - 0 to 13 inches: very stony fine sandy loam

H2 - 13 to 36 inches: fine sandy loam

H3 - 36 to 40 inches: gravelly loamy sand

#### **Properties and qualities**

Slope: 3 to 8 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: A Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

#### Minor Components

#### Rock outcrop

*Percent of map unit:* 10 percent *Hydric soil rating:* No

#### Not named

Percent of map unit: 5 percent Hydric soil rating: No

#### Sutton

Percent of map unit: 5 percent Hydric soil rating: No

#### Buxton

Percent of map unit: 5 percent Hydric soil rating: No

#### Leicester

Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes

# HdC—Hollis-Charlton very rocky fine sandy loams, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 9d7n Elevation: 0 to 1,200 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 120 to 240 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Hollis and similar soils:* 40 percent *Charlton and similar soils:* 30 percent *Minor components:* 30 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Hollis**

#### Setting

Parent material: Till

#### **Typical profile**

*H1 - 0 to 14 inches:* very stony fine sandy loam *H2 - 14 to 18 inches:* bedrock

#### **Properties and qualities**

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: 10 to 20 inches to lithic bedrock
Drainage class: Well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Very low (about 2.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: D Ecological site: F144AY033MA - Shallow Dry Till Uplands Hydric soil rating: No

#### **Description of Charlton**

#### Setting

Parent material: Till

#### **Typical profile**

*H1 - 0 to 13 inches:* very stony fine sandy loam *H2 - 13 to 36 inches:* fine sandy loam *H3 - 36 to 40 inches:* gravelly loamy sand

#### **Properties and qualities**

Slope: 8 to 15 percent
Surface area covered with cobbles, stones or boulders: 1.6 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Low (about 5.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: A Ecological site: F144AY034CT - Well Drained Till Uplands Hydric soil rating: No

#### **Minor Components**

#### Rock outcrop

Percent of map unit: 10 percent Hydric soil rating: No

#### Not named

Percent of map unit: 10 percent Hydric soil rating: No

#### Woodbridge

Percent of map unit: 5 percent Hydric soil rating: No

#### Sutton

Percent of map unit: 5 percent Hydric soil rating: No

# Sb—Saugatuck loamy sand

#### Map Unit Setting

National map unit symbol: 9d8r Elevation: 300 to 1,000 feet Mean annual precipitation: 27 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 125 to 240 days Farmland classification: Not prime farmland

#### Map Unit Composition

Saugatuck and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Saugatuck

#### Setting

Landform: Outwash terraces Parent material: Outwash

#### **Typical profile**

H1 - 0 to 4 inches: loamy sand H2 - 4 to 7 inches: sand H3 - 7 to 26 inches: loamy sand H4 - 26 to 42 inches: sand

#### **Properties and qualities**

Slope: 0 to 3 percent
Depth to restrictive feature: 10 to 16 inches to undefined
Drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Very low (about 1.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Hydric soil rating: Yes

#### **Minor Components**

#### Not named wet

Percent of map unit: 15 percent

Landform: Outwash terraces Hydric soil rating: Yes

# SfC—Suffield silt loam, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 9d8v Elevation: 0 to 250 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of statewide importance

#### Map Unit Composition

Suffield and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Suffield**

#### **Typical profile**

H1 - 0 to 19 inches: silt loam H2 - 19 to 28 inches: silt loam H3 - 28 to 41 inches: silty clay

#### Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water capacity: Moderate (about 7.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: F144AY017NH - Well Drained Lake Plain Hydric soil rating: No

#### Minor Components

#### Not named

Percent of map unit: 9 percent Hydric soil rating: No

# Buxton

Percent of map unit: 5 percent Hydric soil rating: No

#### Rock outcrop

Percent of map unit: 1 percent Hydric soil rating: No 1.3. Precipitation tables



NOAA Atlas 14, Volume 10, Version 3 Location name: Durham, New Hampshire, USA\* Latitude: 43.1354°, Longitude: -70.9281° Elevation: 55.98 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

# PF tabular

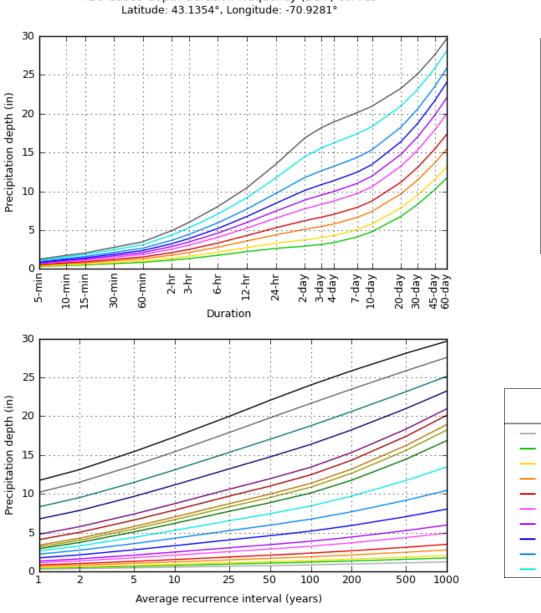
PDS-k	DS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>									
Dunation		Average recurrence interval (years)								
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.300</b> (0.242-0.374)	<b>0.363</b> (0.293-0.453)	<b>0.466</b> (0.374-0.584)	<b>0.550</b> (0.439-0.693)	<b>0.667</b> (0.512-0.877)	<b>0.755</b> (0.565-1.01)	<b>0.847</b> (0.613-1.18)	<b>0.952</b> (0.648-1.35)	<b>1.10</b> (0.718-1.62)	<b>1.23</b> (0.776-1.84)
10-min	<b>0.425</b> (0.343-0.531)	<b>0.514</b> (0.415-0.642)	<b>0.659</b> (0.529-0.825)	<b>0.779</b> (0.622-0.982)	<b>0.945</b> (0.725-1.24)	<b>1.07</b> (0.802-1.44)	<b>1.20</b> (0.869-1.67)	<b>1.35</b> (0.917-1.92)	<b>1.56</b> (1.02-2.30)	<b>1.74</b> (1.10-2.61)
15-min	<b>0.500</b> (0.404-0.624)	<b>0.605</b> (0.488-0.755)	<b>0.776</b> (0.624-0.972)	<b>0.917</b> (0.731-1.16)	<b>1.11</b> (0.853-1.46)	<b>1.26</b> (0.943-1.69)	<b>1.41</b> (1.02-1.97)	<b>1.59</b> (1.08-2.26)	<b>1.84</b> (1.20-2.70)	<b>2.04</b> (1.29-3.07)
30-min	<b>0.669</b> (0.540-0.834)	<b>0.808</b> (0.652-1.01)	<b>1.03</b> (0.832-1.30)	<b>1.22</b> (0.977-1.54)	<b>1.48</b> (1.14-1.96)	<b>1.68</b> (1.26-2.26)	<b>1.88</b> (1.37-2.63)	<b>2.12</b> (1.44-3.02)	<b>2.47</b> (1.61-3.64)	<b>2.77</b> (1.75-4.15)
60-min	<b>0.837</b> (0.676-1.04)	<b>1.01</b> (0.815-1.26)	<b>1.30</b> (1.04-1.62)	<b>1.53</b> (1.22-1.93)	<b>1.86</b> (1.43-2.45)	<b>2.10</b> (1.58-2.83)	<b>2.36</b> (1.71-3.30)	<b>2.66</b> (1.81-3.79)	<b>3.11</b> (2.02-4.58)	<b>3.49</b> (2.21-5.24)
2-hr	<b>1.12</b> (0.911-1.39)	<b>1.37</b> (1.11-1.69)	<b>1.76</b> (1.43-2.19)	<b>2.09</b> (1.68-2.62)	<b>2.55</b> (1.97-3.34)	<b>2.88</b> (2.18-3.87)	<b>3.25</b> (2.38-4.55)	<b>3.69</b> (2.52-5.22)	<b>4.36</b> (2.84-6.38)	<b>4.94</b> (3.14-7.36)
3-hr	<b>1.33</b> (1.08-1.64)	<b>1.62</b> (1.32-2.00)	<b>2.10</b> (1.70-2.60)	<b>2.50</b> (2.01-3.11)	<b>3.05</b> (2.37-3.99)	<b>3.45</b> (2.62-4.62)	<b>3.89</b> (2.87-5.44)	<b>4.43</b> (3.03-6.24)	<b>5.26</b> (3.44-7.67)	<b>5.97</b> (3.80-8.87)
6-hr	<b>1.74</b> (1.43-2.14)	<b>2.14</b> (1.75-2.63)	<b>2.78</b> (2.27-3.43)	<b>3.32</b> (2.69-4.11)	<b>4.06</b> (3.17-5.28)	<b>4.60</b> (3.52-6.13)	<b>5.20</b> (3.85-7.22)	<b>5.93</b> (4.07-8.30)	<b>7.05</b> (4.62-10.2)	<b>8.03</b> (5.12-11.8)
12-hr	<b>2.22</b> (1.84-2.71)	<b>2.74</b> (2.26-3.34)	<b>3.58</b> (2.94-4.39)	<b>4.29</b> (3.50-5.27)	<b>5.25</b> (4.13-6.79)	<b>5.96</b> (4.58-7.89)	<b>6.74</b> (5.02-9.31)	<b>7.69</b> (5.30-10.7)	<b>9.17</b> (6.03-13.2)	<b>10.4</b> (6.68-15.3)
24-hr	<b>2.63</b> (2.19-3.19)	<b>3.30</b> (2.74-4.00)	<b>4.39</b> (3.63-5.33)	<b>5.29</b> (4.34-6.46)	<b>6.53</b> (5.17-8.41)	<b>7.44</b> (5.76-9.82)	<b>8.44</b> (6.34-11.7)	<b>9.71</b> (6.71-13.4)	<b>11.7</b> (7.72-16.8)	<b>13.5</b> (8.64-19.6)
2-day	<b>2.92</b> (2.44-3.51)	<b>3.74</b> (3.12-4.50)	<b>5.09</b> (4.23-6.14)	<b>6.20</b> (5.12-7.53)	<b>7.74</b> (6.18-9.95)	<b>8.86</b> (6.92-11.7)	<b>10.1</b> (7.69-14.0)	<b>11.8</b> (8.15-16.2)	<b>14.5</b> (9.56-20.6)	<b>16.9</b> (10.9-24.4)
3-day	<b>3.14</b> (2.64-3.76)	<b>4.03</b> (3.38-4.83)	<b>5.47</b> (4.57-6.58)	<b>6.67</b> (5.53-8.06)	<b>8.32</b> (6.66-10.7)	<b>9.52</b> (7.46-12.5)	<b>10.9</b> (8.29-15.0)	<b>12.7</b> (8.78-17.3)	<b>15.6</b> (10.3-22.1)	<b>18.2</b> (11.7-26.3)
4-day	<b>3.38</b> (2.84-4.03)	<b>4.29</b> (3.61-5.13)	<b>5.78</b> (4.84-6.93)	<b>7.02</b> (5.83-8.46)	<b>8.72</b> (7.00-11.1)	<b>9.96</b> (7.83-13.1)	<b>11.4</b> (8.68-15.6)	<b>13.2</b> (9.18-18.0)	<b>16.2</b> (10.8-22.9)	<b>18.9</b> (12.2-27.2)
7-day	<b>4.10</b> (3.47-4.86)	<b>5.05</b> (4.27-6.00)	<b>6.62</b> (5.57-7.89)	<b>7.91</b> (6.61-9.49)	<b>9.70</b> (7.81-12.3)	<b>11.0</b> (8.66-14.3)	<b>12.5</b> (9.52-16.9)	<b>14.3</b> (10.0-19.5)	<b>17.4</b> (11.6-24.5)	<b>20.1</b> (13.0-28.8)
10-day	<b>4.79</b> (4.07-5.66)	<b>5.78</b> (4.90-6.84)	<b>7.40</b> (6.24-8.79)	<b>8.74</b> (7.32-10.4)	<b>10.6</b> (8.54-13.3)	<b>11.9</b> (9.40-15.4)	<b>13.4</b> (10.2-18.1)	<b>15.3</b> (10.7-20.7)	<b>18.3</b> (12.2-25.7)	<b>21.0</b> (13.6-29.9)
20-day	<b>6.76</b> (5.78-7.94)	<b>7.86</b> (6.71-9.25)	<b>9.66</b> (8.21-11.4)	<b>11.2</b> (9.41-13.2)	<b>13.2</b> (10.7-16.4)	<b>14.8</b> (11.6-18.7)	<b>16.4</b> (12.4-21.5)	<b>18.3</b> (12.9-24.5)	<b>21.0</b> (14.1-29.1)	<b>23.3</b> (15.1-32.9)
30-day	<b>8.32</b> (7.14-9.74)	<b>9.52</b> (8.16-11.2)	<b>11.5</b> (9.79-13.5)	<b>13.1</b> (11.1-15.5)	<b>15.3</b> (12.4-18.8)	<b>17.0</b> (13.4-21.3)	<b>18.8</b> (14.1-24.3)	<b>20.6</b> (14.6-27.5)	<b>23.2</b> (15.6-32.0)	<b>25.2</b> (16.4-35.5)
45-day	<b>10.2</b> (8.79-11.9)	<b>11.5</b> (9.90-13.4)	<b>13.7</b> (11.7-16.0)	<b>15.4</b> (13.1-18.2)	<b>17.9</b> (14.5-21.8)	<b>19.8</b> (15.6-24.6)	<b>21.7</b> (16.2-27.7)	<b>23.5</b> (16.7-31.2)	<b>25.9</b> (17.5-35.6)	<b>27.6</b> (18.0-38.8)
60-day	<b>11.7</b> (10.1-13.6)	<b>13.1</b> (11.3-15.3)	<b>15.4</b> (13.3-18.0)	<b>17.3</b> (14.8-20.4)	<b>20.0</b> (16.2-24.2)	<b>22.1</b> (17.4-27.2)	<b>24.0</b> (18.0-30.5)	<b>25.9</b> (18.4-34.2)	<b>28.1</b> (19.0-38.5)	<b>29.7</b> (19.4-41.6)

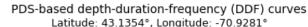
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

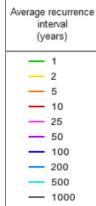
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

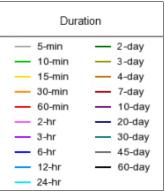
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**PF graphical** 









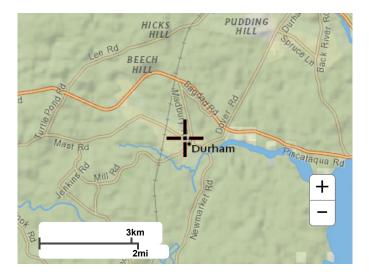
NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Fri Jun 17 05:04:28 2022

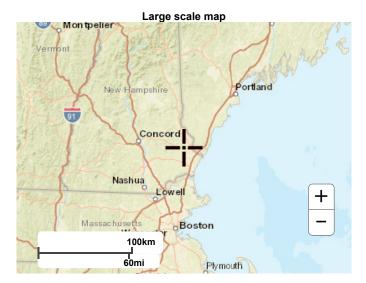
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Maps & aerials

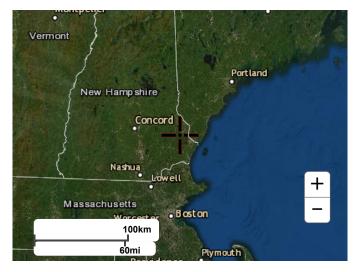
Small scale terrain







Large scale aerial



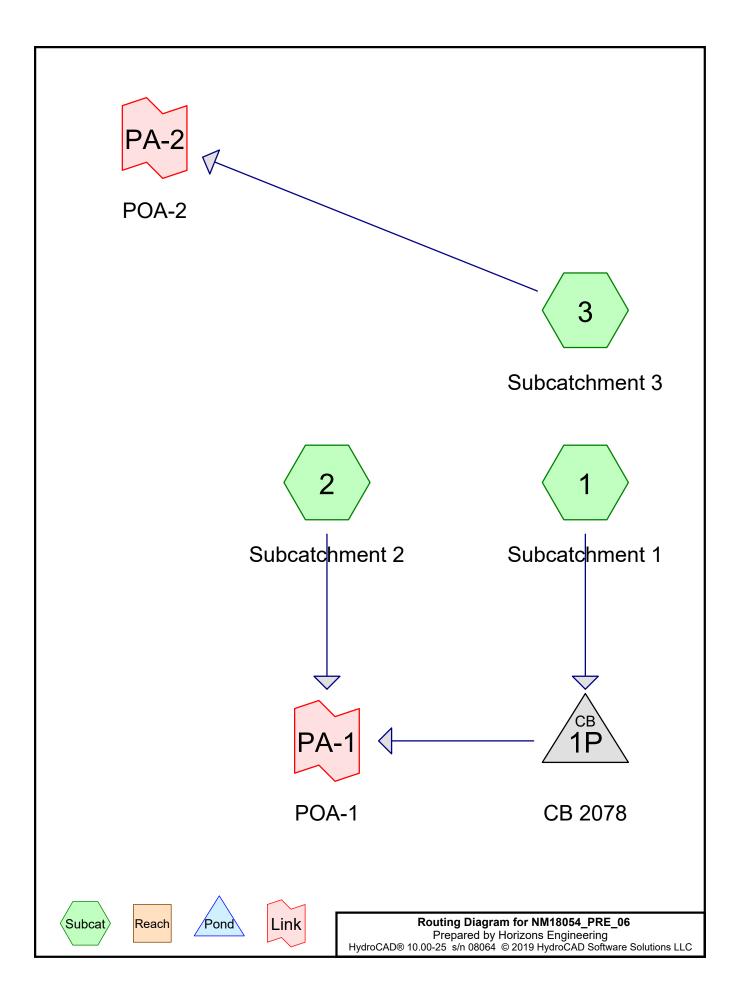
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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

**Disclaimer** 

2. DRAINAGE CALCULATIONS

2.1. Pre-development analysis



# Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
8,902	74	>75% Grass cover, Good, HSG C (1, 2, 3)
18,468	98	Paved parking & roofs, HSG C (1, 2, 3)
2,892	98	Paved parking, HSG C (1, 2, 3)
30,262	91	TOTAL AREA

NH-Durham(NOAA) 24-hr S1 1-yr 1" Rainfall=1.00"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 2 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Subcatchment 1	Runoff Area=14,023 sf 82.49% Impervious Runoff Depth=0.66" Tc=6.0 min CN=WQ Runoff=0.26 cfs 767 cf
Subcatchment 2: Subcatchment 2	Runoff Area=2,059 sf 47.50% Impervious Runoff Depth=0.39" Tc=6.0 min CN=WQ Runoff=0.02 cfs 67 cf
Subcatchment 3: Subcatchment 3	Runoff Area=14,180 sf 62.17% Impervious Runoff Depth=0.50" Tc=6.0 min CN=WQ Runoff=0.19 cfs 591 cf
Pond 1P: CB 2078	$\label{eq:Peak Elev=50.25' Inflow=0.26 cfs 767 cf} Peak Elev=50.25' Inflow=0.26 cfs 767 cf 12.0'' Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=0.26 cfs 767 cf$
Link PA-1: POA-1	Inflow=0.28 cfs 834 cf Primary=0.28 cfs 834 cf
Link PA-2: POA-2	Inflow=0.19 cfs 591 cf Primary=0.19 cfs 591 cf

#### Total Runoff Area = 30,262 sf Runoff Volume = 1,425 cf Average Runoff Depth = 0.57" 29.42% Pervious = 8,902 sf 70.58% Impervious = 21,360 sf

NH-Durham(NOAA) 24-hr S1 2-yr Rainfall=3.30"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 2 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Subcatchment 1	Runoff Area=14,023 sf 82.49% Impervious Runoff Depth=2.72" Tc=6.0 min CN=WQ Runoff=0.96 cfs 3,182 cf
Subcatchment 2: Subcatchment 2	Runoff Area=2,059 sf 47.50% Impervious Runoff Depth=2.04" Tc=6.0 min CN=WQ Runoff=0.11 cfs 349 cf
Subcatchment 3: Subcatchment 3	Runoff Area=14,180 sf 62.17% Impervious Runoff Depth=2.32" Tc=6.0 min CN=WQ Runoff=0.83 cfs 2,747 cf
Pond 1P: CB 2078	Peak Elev=50.50' Inflow=0.96 cfs 3,182 cf 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=0.96 cfs 3,182 cf
Link PA-1: POA-1	Inflow=1.07 cfs 3,532 cf Primary=1.07 cfs 3,532 cf
Link PA-2: POA-2	Inflow=0.83 cfs 2,747 cf Primary=0.83 cfs 2,747 cf

Total Runoff Area = 30,262 sf Runoff Volume = 6,278 cf Average Runoff Depth = 2.49" 29.42% Pervious = 8,902 sf 70.58% Impervious = 21,360 sf

NH-Durham(NOAA) 24-hr S1 25-yr Rainfall=6.53"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 2 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Subcatchment	L Runoff Area=14,023 sf 82.49% Impervious Runoff Depth=5.83" Tc=6.0 min CN=WQ Runoff=1.88 cfs 6,808 cf
Subcatchment 2: Subcatchment 2	2 Runoff Area=2,059 sf 47.50% Impervious Runoff Depth=4.90" Tc=6.0 min CN=WQ Runoff=0.24 cfs 840 cf
Subcatchment 3: Subcatchment 3	Runoff Area=14,180 sf 62.17% Impervious Runoff Depth=5.29" Tc=6.0 min CN=WQ Runoff=1.76 cfs 6,247 cf
Pond 1P: CB 2078	$\label{eq:Peak Elev=50.75'} Peak Elev=50.75' Inflow=1.88 \mbox{ cfs } 6,808 \mbox{ cf} 12.0'' Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=1.88 \mbox{ cfs } 6,808 \mbox{ cf} \end{tabular}$
Link PA-1: POA-1	Inflow=2.12 cfs 7,649 cf Primary=2.12 cfs 7,649 cf
Link PA-2: POA-2	Inflow=1.76 cfs 6,247 cf Primary=1.76 cfs 6,247 cf

Total Runoff Area = 30,262 sf Runoff Volume = 13,895 cf Average Runoff Depth = 5.51" 29.42% Pervious = 8,902 sf 70.58% Impervious = 21,360 sf

NH-Durham(NOAA) 24-hr S1 50-yr Rainfall=7.44"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 2 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Subcatchment	L Runoff Area=14,023 sf 82.49% Impervious Runoff Depth=6.71" Tc=6.0 min CN=WQ Runoff=2.15 cfs 7,847 cf
Subcatchment 2: Subcatchment 2	2 Runoff Area=2,059 sf 47.50% Impervious Runoff Depth=5.74" Tc=6.0 min CN=WQ Runoff=0.28 cfs 986 cf
Subcatchment 3: Subcatchment 3	Runoff Area=14,180 sf 62.17% Impervious Runoff Depth=6.15" Tc=6.0 min CN=WQ Runoff=2.03 cfs 7,269 cf
Pond 1P: CB 2078	$\label{eq:Peak Elev=50.83'} Peak Elev=50.83' Inflow=2.15 \mbox{ cfs } 7,847 \mbox{ cf} 12.0'' Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=2.15 \mbox{ cfs } 7,847 \mbox{ cf} 12.0'' Round Culvert n=0.012 L=90.0' S=0.0100 '/' Round Culvert n=0.012 Round$
Link PA-1: POA-1	Inflow=2.43 cfs 8,833 cf Primary=2.43 cfs 8,833 cf
Link PA-2: POA-2	Inflow=2.03 cfs 7,269 cf Primary=2.03 cfs 7,269 cf

#### Total Runoff Area = 30,262 sf Runoff Volume = 16,102 cf Average Runoff Depth = 6.39" 29.42% Pervious = 8,902 sf 70.58% Impervious = 21,360 sf

NH-Durham(NOAA) 24-hr S1 100-yr Rainfall=8.44"

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Time span=0.00-48.00 hrs, dt=0.01 hrs, 4801 points x 2 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1: Subcatchment	Runoff Area=14,023 sf 82.49% Impervious Runoff Depth=7.70" Tc=6.0 min CN=WQ Runoff=2.43 cfs 8,993 cf
Subcatchment 2: Subcatchment 2	2 Runoff Area=2,059 sf 47.50% Impervious Runoff Depth=6.69" Tc=6.0 min CN=WQ Runoff=0.32 cfs 1,148 cf
Subcatchment 3: Subcatchment 3	Runoff Area=14,180 sf 62.17% Impervious Runoff Depth=7.11" Tc=6.0 min CN=WQ Runoff=2.32 cfs 8,402 cf
Pond 1P: CB 2078	eq:Peak Elev=50.91' Inflow=2.43 cfs \$ 8,993 cf \$ 12.0'' Round Culvert \$ n=0.012 L=90.0' S=0.0100 '/' Outflow=2.43 cfs \$ 8,993 cf \$ 12.0'' Round Culvert \$ n=0.012 L=90.0' S=0.0100 '/' \$ 0000000000000000000000000000000
Link PA-1: POA-1	Inflow=2.75 cfs 10,141 cf Primary=2.75 cfs 10,141 cf
Link PA-2: POA-2	Inflow=2.32 cfs 8,402 cf Primary=2.32 cfs 8,402 cf

#### Total Runoff Area = 30,262 sf Runoff Volume = 18,543 cf Average Runoff Depth = 7.35" 29.42% Pervious = 8,902 sf 70.58% Impervious = 21,360 sf

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Page 1

# Summary for Subcatchment 1: Subcatchment 1

Runoff = 1.52 cfs @ 12.04 hrs, Volume= 5,402 cf, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

Are	ea (sf)	CN	CN Description						
	21	74	>75% Grass	s cover, Go	ood, HSG C				
	2,435	74	>75% Grass	s cover, Go	ood, HSG C				
	147	98	Paved parkin	ng, HSG C					
1	L1,420	98	Paved parki	ng & roofs,	s, HSG C				
1	14,023 Weighted Average								
	2,456 17.51% Pervious Area								
1	11,567 82.49% Impervious Area				rea				
Tc	Length	Slop	,	Capacity					
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					
6.0					Direct Entry,				

# Summary for Subcatchment 2: Subcatchment 2

Runoff = 0.19 cfs @ 12.04 hrs, Volume= 646 cf, Depth= 3.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

Area	(sf)	CN	CN Description					
	123	74	>75% Grass	s cover, Go	od, HSG C			
	958	74	>75% Grass	s cover, Go	od, HSG C			
	310	98	Paved parki	ng, HSG C				
	668	98	Paved parki	ng & roofs,	HSG C			
2,	2,059 Weighted Average							
1,	,081		52.50% Per	vious Area				
	978 47.50% Impervious Area							
Tc Le	ength	Slop	e Velocity	Capacity	Description			
(min) (	(feet)	(ft/f	:) (ft/sec)	(cfs)				
6.0					Direct Entry,			

# Summary for Subcatchment 3: Subcatchment 3

Runoff = 1.40 cfs @ 12.04 hrs, Volume= 4,873 cf, Depth= 4.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

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	Area (sf)	CN	Description					
	658	74	>75% Grass cover, Good, HSG C					
	4,707	74	>75% Grass cover, Good, HSG C					
	2,435	98	Paved parking, HSG C					
	6,380							
14,180 Weighted Average								
	5,365 37.83% Pervious Area							
8,815 62.17% Impervious Area								
	Tc Length	Slo	, , , , ,					
	(min) (feet)	(ft/	ft) (ft/sec) (cfs)					
	6.0		Direct Entry					

6.0

Direct Entry,

#### Summary for Pond 1P: CB 2078

[57] Hint: Peaked at 50.66' (Flood elevation advised)

Inflow Area =	14,023 sf, 82.49% Impervious,	Inflow Depth =	4.62" for 10-yr event
Inflow =	1.52 cfs @ 12.04 hrs, Volume=	5,402 cf	
Outflow =	1.52 cfs @ 12.04 hrs, Volume=	5,402 cf,	Atten= 0%, Lag= 0.0 min
Primary =	1.52 cfs @ 12.04 hrs, Volume=	5,402 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 2 Peak Elev= 50.66' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	50.00'	<b>12.0"</b> Round Outlet L= 90.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.00' / 49.10' S= 0.0100 '/' Cc= 0.900 n= 0.012 Concrete pipe, finished, Flow Area= 0.79 sf

**Primary OutFlow** Max=1.52 cfs @ 12.04 hrs HW=50.66' TW=0.00' (Dynamic Tailwater) **1=Outlet** (Inlet Controls 1.52 cfs @ 2.76 fps)

# Summary for Link PA-1: POA-1

Inflow Area =		16,082 s	f, 78.01% I	Impervious,	Inflow Depth =	4.51"	for	10-yr event
Inflow	=	1.71 cfs @	12.04 hrs,	Volume=	6,048 cf			
Primary	=	1.71 cfs @	12.04 hrs,	Volume=	6,048 cf,	Atten=	0%,	Lag= 0.0 min

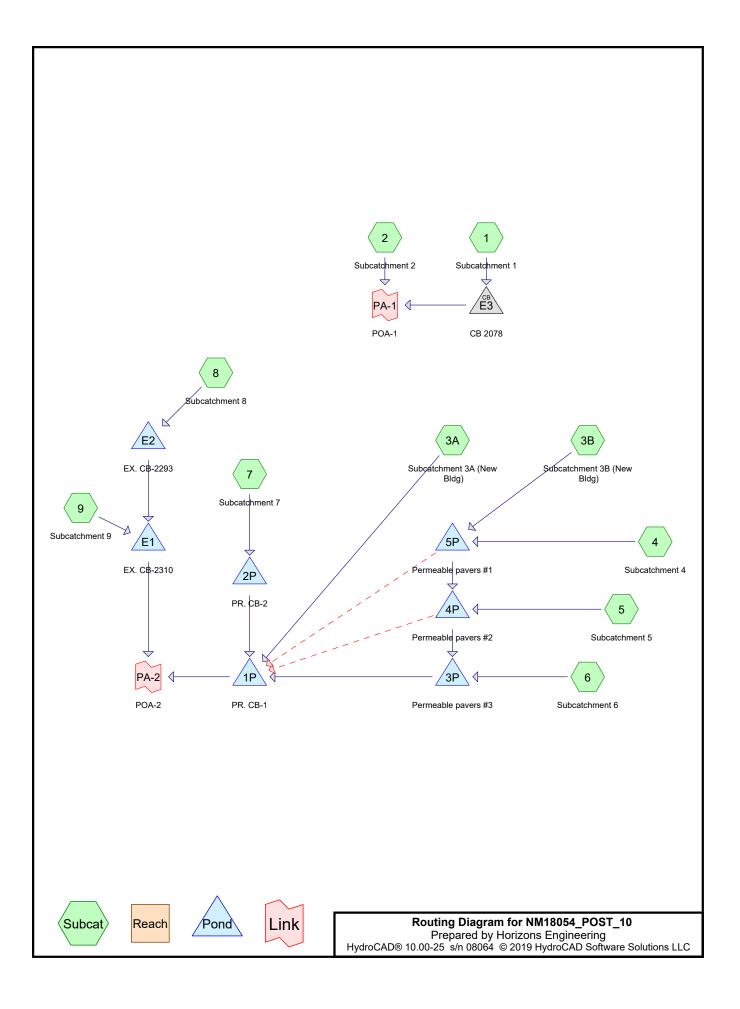
Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

# Summary for Link PA-2: POA-2

Inflow Area =		14,180 s	f, 62.17% I	impervious,	Inflow Depth =	4.12"	for	10-yr event
Inflow	=	1.40 cfs @	12.04 hrs,	Volume=	4,873 cf			
Primary	=	1.40 cfs @	12.04 hrs,	Volume=	4,873 cf,	Atten=	0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs

2.2. Post-development analysis



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# Area Listing (all nodes)

Area	CN	Description		
(sq-ft)		(subcatchment-numbers)		
5,386	74	>75% Grass cover, Good, HSG C (1, 2)		
9,265	98	Paved parking & roofs, HSG C (1, 2)		
9,372	98	Paved parking, HSG C (1, 2, 4, 5, 6, 7, 8, 9)		
6,301	98	Roofs, HSG C (3A, 3B)		
30,324	94	TOTAL AREA		

NH-Durham(NOAA) 24-hr S1 1-yr 1" Rainfall=1.00"

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method								
Subcatchment 1: Subcatchment 1	Runoff Area=13,022 sf 70.32% Impervious Runoff Depth=0.56" Tc=6.0 min CN=WQ Runoff=0.20 cfs 611 cf							
Subcatchment 2: Subcatchment 2	Runoff Area=2,499 sf 39.14% Impervious Runoff Depth=0.32" Tc=6.0 min CN=WQ Runoff=0.02 cfs 67 cf							
Subcatchment 3A: Subcatchment 3A (N	ew Runoff Area=2,301 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.05 cfs 152 cf							
Subcatchment 3B: Subcatchment 3B (N	ew Runoff Area=4,000 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.09 cfs 264 cf							
Subcatchment 4: Subcatchment 4	Runoff Area=383 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.01 cfs 25 cf							
Subcatchment 5: Subcatchment 5	Runoff Area=937 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.02 cfs 62 cf							
Subcatchment 6: Subcatchment 6	Runoff Area=803 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.02 cfs 53 cf							
Subcatchment 7: Subcatchment 7	Runoff Area=3,476 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.08 cfs 229 cf							
Subcatchment 8: Subcatchment 8	Runoff Area=2,572 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.06 cfs 170 cf							
Subcatchment 9: Subcatchment 9	Runoff Area=331 sf 100.00% Impervious Runoff Depth=0.79" Tc=6.0 min CN=98 Runoff=0.01 cfs 22 cf							
Pond 1P: PR. CB-1 12.0'	Peak Elev=47.70' Storage=9 cf Inflow=0.13 cfs 374 cf Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.13 cfs 368 cf							
Pond 2P: PR. CB-2 12.0'	Peak Elev=47.76' Storage=10 cf Inflow=0.08 cfs 229 cf Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.08 cfs 223 cf							
Pond 3P: Permeable pavers #3	Peak Elev=50.12' Storage=14 cf Inflow=0.02 cfs 53 cf Discarded=0.00 cfs 53 cf Primary=0.00 cfs 0 cf Outflow=0.00 cfs 53 cf							
Pond 4P: Permeable pavers #2 Discarded=0.00 cfs 62 cf	Peak Elev=50.35' Storage=19 cf Inflow=0.02 cfs 62 cf Primary=0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.00 cfs 62 cf							
Pond 5P: Permeable pavers #1 Discarded=0.01 cfs 289 cf P	Peak Elev=52.05' Storage=127 cf Inflow=0.10 cfs 289 cf rimary=0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.01 cfs 289 cf							
Pond E1: EX. CB-2310	Peak Elev=47.64' Storage=8 cf Inflow=0.06 cfs 185 cf Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.06 cfs 179 cf							

NH-Durham(NOAA) 24-hr S1 1-yr 1" Rainfall=1.00"

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Pond E2: EX. CB-2293	Peak Elev=47.72' Storage=9 cf Inflow=0.06 c 12.0" Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.06 c	
Pond E3: CB 2078	Peak Elev=50.22' Inflow=0.20 of 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=0.20 of 12.0"	
Link PA-1: POA-1	Inflow=0.22 o Primary=0.22 o	
Link PA-2: POA-2	Inflow=0.19 o Primary=0.19 o	

Total Runoff Area = 30,324 sf Runoff Volume = 1,654 cf Average Runoff Depth = 0.65" 17.76% Pervious = 5,386 sf 82.24% Impervious = 24,938 sf

NH-Durham(NOAA) 24-hr S1 2-yr Rainfall=3.30"

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method							
Subcatchment 1: Subcatchment 1	Runoff Area=13,022 sf 70.32% Impervious Runoff Depth=2.48" Tc=6.0 min CN=WQ Runoff=0.81 cfs 2,696 cf						
Subcatchment 2: Subcatchment 2	Runoff Area=2,499 sf 39.14% Impervious Runoff Depth=1.87" Tc=6.0 min CN=WQ Runoff=0.12 cfs 390 cf						
Subcatchment 3A: Subcatchment 3A (New	Runoff Area=2,301 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.18 cfs 588 cf						
Subcatchment 3B: Subcatchment 3B (New	Runoff Area=4,000 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.31 cfs 1,022 cf						
Subcatchment 4: Subcatchment 4	Runoff Area=383 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.03 cfs 98 cf						
Subcatchment 5: Subcatchment 5	Runoff Area=937 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.07 cfs 239 cf						
Subcatchment 6: Subcatchment 6	Runoff Area=803 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.06 cfs 205 cf						
Subcatchment 7: Subcatchment 7	Runoff Area=3,476 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.27 cfs 888 cf						
Subcatchment 8: Subcatchment 8	Runoff Area=2,572 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.20 cfs 657 cf						
Subcatchment 9: Subcatchment 9	Runoff Area=331 sf 100.00% Impervious Runoff Depth=3.07" Tc=6.0 min CN=98 Runoff=0.03 cfs 85 cf						
Pond 1P: PR. CB-1 12.0" Round	Peak Elev=47.91' Storage=11 cf Inflow=0.55 cfs 1,939 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.55 cfs 1,932 cf						
Pond 2P: PR. CB-2 12.0" Roun	Peak Elev=47.99' Storage=12 cf Inflow=0.27 cfs 888 cf d Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.27 cfs 882 cf						
Pond 3P: Permeable pavers #3 Discarded	Peak Elev=50.33' Storage=62 cf Inflow=0.06 cfs 205 cf I=0.01 cfs 205 cf Primary=0.00 cfs 0 cf Outflow=0.01 cfs 205 cf						
Pond 4P: Permeable pavers #2 Discarded=0.01 cfs 288 cf Primary	Peak Elev=51.01' Storage=138 cf Inflow=0.27 cfs 288 cf =0.00 cfs 0 cf Secondary=0.00 cfs 0 cf Outflow=0.01 cfs 288 cf						
Pond 5P: Permeable pavers #1 Discarded=0.01 cfs 604 cf Primary=0.20	Peak Elev=52.52' Storage=267 cf Inflow=0.34 cfs 1,120 cf cfs 48 cf Secondary=0.11 cfs 468 cf Outflow=0.32 cfs 1,120 cf						
Pond E1: EX. CB-2310	Peak Elev=47.76' Storage=10 cf Inflow=0.22 cfs 736 cf						

12.0" Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.22 cfs 729 cf

NH-Durham(NOAA) 24-hr S1 2-yr Rainfall=3.30"

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Pond E2: EX. CB-2293	Peak Elev=47.87' Storage=11 cf Inflow=0.20 cfs 657 cf 12.0" Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.20 cfs 651 cf					
Pond E3: CB 2078	Peak Elev=50.46' Inflow=0.81 cfs 2,696 cf 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=0.81 cfs 2,696 cf					
Link PA-1: POA-1	Inflow=0.93 cfs 3,086 cf Primary=0.93 cfs 3,086 cf					
Link PA-2: POA-2	Inflow=0.77 cfs 2,662 cf Primary=0.77 cfs 2,662 cf					

# Total Runoff Area = 30,324 sf Runoff Volume = 6,869 cf Average Runoff Depth = 2.72" 17.76% Pervious = 5,386 sf 82.24% Impervious = 24,938 sf

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method							
Subcatchment 1: Subcatchment 1	Runoff Area=13,022 sf 70.32% Impervious Runoff Depth=5.50" Tc=6.0 min CN=WQ Runoff=1.67 cfs 5,972 cf						
Subcatchment 2: Subcatchment 2	Runoff Area=2,499 sf 39.14% Impervious Runoff Depth=4.67" Tc=6.0 min CN=WQ Runoff=0.28 cfs 974 cf						
Subcatchment 3A: Subcatchment 3A (New	Runoff Area=2,301 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.33 cfs 1,206 cf						
Subcatchment 3B: Subcatchment 3B (New	Runoff Area=4,000 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.57 cfs 2,097 cf						
Subcatchment 4: Subcatchment 4	Runoff Area=383 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.05 cfs 201 cf						
Subcatchment 5: Subcatchment 5	Runoff Area=937 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.13 cfs 491 cf						
Subcatchment 6: Subcatchment 6	Runoff Area=803 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.11 cfs 421 cf						
Subcatchment 7: Subcatchment 7	Runoff Area=3,476 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.50 cfs 1,822 cf						
Subcatchment 8: Subcatchment 8	Runoff Area=2,572 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.37 cfs 1,348 cf						
Subcatchment 9: Subcatchment 9	Runoff Area=331 sf 100.00% Impervious Runoff Depth=6.29" Tc=6.0 min CN=98 Runoff=0.05 cfs 174 cf						
Pond 1P: PR. CB-1 12.0" Round	Peak Elev=48.08' Storage=14 cf Inflow=1.00 cfs 4,555 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=1.00 cfs 4,548 cf						
Pond 2P: PR. CB-2 12.0" Round	Peak Elev=48.18' Storage=15 cf Inflow=0.50 cfs 1,822 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.49 cfs 1,816 cf						
Pond 3P: Permeable pavers #3 Discarded	Peak Elev=50.87' Storage=235 cf Inflow=0.50 cfs 511 cf I=0.01 cfs 511 cf Primary=0.00 cfs 0 cf Outflow=0.01 cfs 511 cf						
Pond 4P: Permeable pavers #2 Discarded=0.01 cfs 473 cf Primary=0.	Peak Elev=51.53' Storage=278 cf Inflow=0.64 cfs 759 cf 41 cfs 90 cf Secondary=0.11 cfs 196 cf Outflow=0.53 cfs 759 cf						
Pond 5P: Permeable pavers #1 Discarded=0.01 cfs 694 cf Primary=0.50 cfs	Peak Elev=52.53' Storage=272 cf Inflow=0.62 cfs 2,298 cf s 268 cf Secondary=0.11 cfs 1,336 cf Outflow=0.62 cfs 2,298 cf						
Pond E1: EX. CB-2310 12.0" Round	Peak Elev=47.86' Storage=11 cf Inflow=0.41 cfs 1,516 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.41 cfs 1,509 cf						

Pond E2: EX. CB-2293

NH-Durham(NOAA) 24-hr S1 25-yr Rainfall=6.53"

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Peak Elev=50.70' Inflow=1.67 cfs 5,972 cf 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=1.67 cfs 5,972 cf

Inflow=1.95 cfs 6,945 cf Primary=1.95 cfs 6,945 cf

Link PA-2: POA-2

Pond E3: CB 2078

Link PA-1: POA-1

Inflow=1.41 cfs 6,058 cf Primary=1.41 cfs 6,058 cf

Total Runoff Area = 30,324 sf Runoff Volume = 14,706 cf Average Runoff Depth = 5.82" 17.76% Pervious = 5,386 sf 82.24% Impervious = 24,938 sf

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method							
Subcatchment 1: Subcatchment 1	Runoff Area=13,022 sf 70.32% Impervious Runoff Depth=6.38" Tc=6.0 min CN=WQ Runoff=1.92 cfs 6,921 cf						
Subcatchment 2: Subcatchment 2	Runoff Area=2,499 sf 39.14% Impervious Runoff Depth=5.51" Tc=6.0 min CN=WQ Runoff=0.33 cfs 1,148 cf						
Subcatchment 3A: Subcatchment 3A (New	Runoff Area=2,301 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.37 cfs 1,381 cf						
Subcatchment 3B: Subcatchment 3B (New	Runoff Area=4,000 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.65 cfs 2,400 cf						
Subcatchment 4: Subcatchment 4	Runoff Area=383 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.06 cfs 230 cf						
Subcatchment 5: Subcatchment 5	Runoff Area=937 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.15 cfs 562 cf						
Subcatchment 6: Subcatchment 6	Runoff Area=803 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.13 cfs 482 cf						
Subcatchment 7: Subcatchment 7	Runoff Area=3,476 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.56 cfs 2,086 cf						
Subcatchment 8: Subcatchment 8	Runoff Area=2,572 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.42 cfs 1,543 cf						
Subcatchment 9: Subcatchment 9	Runoff Area=331 sf 100.00% Impervious Runoff Depth=7.20" Tc=6.0 min CN=98 Runoff=0.05 cfs 199 cf						
Pond 1P: PR. CB-1 12.0" Round	Peak Elev=48.13' Storage=14 cf Inflow=1.15 cfs 5,325 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=1.15 cfs 5,318 cf						
Pond 2P: PR. CB-2 12.0" Round	Peak Elev=48.23' Storage=15 cf Inflow=0.56 cfs 2,086 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.56 cfs 2,079 cf						
Pond 3P: Permeable pavers #3 Discarded=	Peak Elev=51.10' Storage=309 cf Inflow=0.83 cfs 657 cf =0.01 cfs 603 cf Primary=0.04 cfs 54 cf Outflow=0.05 cfs 657 cf						
Pond 4P: Permeable pavers #2 Discarded=0.01 cfs 501 cf Primary=0.70	Peak Elev=51.54' Storage=281 cf Inflow=0.74 cfs 904 cf 0 cfs 175 cf Secondary=0.11 cfs 228 cf Outflow=0.82 cfs 904 cf						
Pond 5P: Permeable pavers #1 Discarded=0.01 cfs 706 cf Primary=0.59 cfs	Peak Elev=52.53' Storage=273 cf Inflow=0.71 cfs 2,630 cf s 341 cf Secondary=0.11 cfs 1,583 cf Outflow=0.71 cfs 2,630 cf						
Pond E1: EX. CB-2310	Peak Elev=47.88' Storage=11 cf Inflow=0.47 cfs 1,736 cf						

 Peak Elev=47.88' Storage=11 cf Inflow=0.47 cfs 1,736 cf

 12.0" Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.47 cfs 1,729 cf

NH-Durham(NOAA) 24-hr S1 50-yr Rainfall=7.44"

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Pond E2: EX. CB-2293	Peak Elev=48.03' Storage	=13 cf Inflow=0.42 cfs 1,543 cf					
	12.0" Round Culvert n=0.025 L=22.4' S=0.02	23 '/' Outflow=0.41 cfs 1,537 cf					

Peak Elev=50.76' Inflow=1.92 cfs 6,921 cf 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=1.92 cfs 6,921 cf

> Inflow=2.25 cfs 8,069 cf Primary=2.25 cfs 8,069 cf

Link PA-2: POA-2

Pond E3: CB 2078

Link PA-1: POA-1

Inflow=1.62 cfs 7,048 cf Primary=1.62 cfs 7,048 cf

Total Runoff Area = 30,324 sf Runoff Volume = 16,951 cf Average Runoff Depth = 6.71" 17.76% Pervious = 5,386 sf 82.24% Impervious = 24,938 sf

NH-Durham(NOAA) 24-hr S1 100-yr Rainfall=8.44"

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method							
Subcatchment 1: Subcatchment 1	Runoff Area=13,022 sf 70.32% Impervious Runoff Depth=7.35" Tc=6.0 min CN=WQ Runoff=2.18 cfs 7,971 cf						
Subcatchment 2: Subcatchment 2	Runoff Area=2,499 sf 39.14% Impervious Runoff Depth=6.45" Tc=6.0 min CN=WQ Runoff=0.38 cfs 1,343 cf						
Subcatchment 3A: Subcatchment 3A (New	Runoff Area=2,301 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.42 cfs 1,572 cf						
Subcatchment 3B: Subcatchment 3B (New	Runoff Area=4,000 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.73 cfs 2,733 cf						
Subcatchment 4: Subcatchment 4	Runoff Area=383 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.07 cfs 262 cf						
Subcatchment 5: Subcatchment 5	Runoff Area=937 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.17 cfs 640 cf						
Subcatchment 6: Subcatchment 6	Runoff Area=803 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.15 cfs 549 cf						
Subcatchment 7: Subcatchment 7	Runoff Area=3,476 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.63 cfs 2,375 cf						
Subcatchment 8: Subcatchment 8	Runoff Area=2,572 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.47 cfs 1,758 cf						
Subcatchment 9: Subcatchment 9	Runoff Area=331 sf 100.00% Impervious Runoff Depth=8.20" Tc=6.0 min CN=98 Runoff=0.06 cfs 226 cf						
Pond 1P: PR. CB-1 12.0" Round	Peak Elev=48.17' Storage=15 cf Inflow=1.27 cfs 6,243 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=1.27 cfs 6,237 cf						
Pond 2P: PR. CB-2 12.0" Round	Peak Elev=48.27' Storage=16 cf Inflow=0.63 cfs 2,375 cf Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.63 cfs 2,369 cf						
Pond 3P: Permeable pavers #3 Discarded=	Peak Elev=51.34' Storage=387 cf Inflow=0.95 cfs 822 cf 0.01 cfs 637 cf Primary=0.11 cfs 184 cf Outflow=0.12 cfs 822 cf						
Pond 4P: Permeable pavers #2 Discarded=0.01 cfs 528 cf Primary=0.80	Peak Elev=51.54' Storage=282 cf Inflow=0.84 cfs 1,066 cf cfs 273 cf Secondary=0.11 cfs 265 cf Outflow=0.92 cfs 1,066 cf						
Pond 5P: Permeable pavers #1 Discarded=0.01 cfs 717 cf Primary=0.67 cfs	Peak Elev=52.54' Storage=274 cf Inflow=0.79 cfs 2,995 cf s 426 cf Secondary=0.11 cfs 1,853 cf Outflow=0.79 cfs 2,995 cf						
Pond E1: EX. CB-2310	Peak Elev=47.91' Storage=11 cf Inflow=0.53 cfs 1,977 cf						

 Pond E1: EX. CB-2310
 Peak Elev=47.91'
 Storage=11 cf
 Inflow=0.53 cfs
 1,977 cf

 12.0"
 Round Culvert
 n=0.025
 L=22.4'
 S=0.0223 '/'
 Outflow=0.53 cfs
 1,971 cf

NH-Durham(NOAA) 24-hr S1 100-yr Rainfall=8.44"

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Pond E2: EX. CB-2293	Peak Elev=48.06' Storage=13 cf Inflow=0.47 cfs 1,758 cf 12.0" Round Culvert n=0.025 L=22.4' S=0.0223 '/' Outflow=0.47 cfs 1,751 cf				
Pond E3: CB 2078	Peak Elev=50.84' Inflow=2.18 cfs 7,971 cf 12.0" Round Culvert n=0.012 L=90.0' S=0.0100 '/' Outflow=2.18 cfs 7,971 cf				
Link PA-1: POA-1	Inflow=2.57 cfs 9,314 cf Primary=2.57 cfs 9,314 cf				
Link PA-2: POA-2	Inflow=1.80 cfs 8,208 cf Primary=1.80 cfs 8,208 cf				

Total Runoff Area = 30,324 sf Runoff Volume = 19,429 cf Average Runoff Depth = 7.69" 17.76% Pervious = 5,386 sf 82.24% Impervious = 24,938 sf

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#### Summary for Subcatchment 1: Subcatchment 1

Runoff = 1.34 cfs @ 12.04 hrs, Volume= 4,692 cf, Depth= 4.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

Are	a (sf)	CN	Description						
	21	74	>75	5% Grass	cover, Go	d, HSG C			
	3,844	74	>75	5% Grass	cover, Go	d, HSG C			
	560	98	Pav	ed parkir	ng, HSG C				
	8,597	98	Pav	ed parkir	ng & roofs,	HSG C			
1	3,022		Weighted Average						
	3,865		29.68% Pervious Area						
	9,157		70.32% Impervious Area						
Tc I	Length	Slo		Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/	t)	(ft/sec)	(cfs)				
6.0						Direct Entry,			

# Summary for Subcatchment 2: Subcatchment 2

Runoff = 0.22 cfs @ 12.04 hrs, Volume= 741 cf, Depth= 3.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

Are	ea (sf)	CN	Description						
	123	74	>75% Grass	s cover, Go	od, HSG C				
	1,398	74	>75% Grass	s cover, Go	od, HSG C				
	310	98	Paved parki	ng, HSG C					
	668	98	Paved parki	ng & roofs,	HSG C				
	2,499		Weighted Average						
	1,521		60.86% Pervious Area						
	978		39.14% Impervious Area						
Тс	Length	Slop		Capacity	Description				
(min)	(feet)	(ft/f	:) (ft/sec)	(cfs)					
6.0					Direct Entry,				

#### Summary for Subcatchment 3A: Subcatchment 3A (New Bldg)

Runoff = 0.27 cfs @ 12.04 hrs, Volume= 969 cf, Depth= 5.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

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Area (sf)	CN	Description		
2,301	98	Roofs, HSG	С	
2,301		100.00% Im	npervious A	Area
Tc Length (min) (feet)	Slo (ft/	be Velocity (ft) (ft/sec)	Capacity (cfs)	•
6.0				Direct Entry,

# Summary for Subcatchment 3B: Subcatchment 3B (New Bldg)

Runoff = 0.47 cfs @ 12.04 hrs, Volume= 1,684 cf, Depth= 5.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

A	rea (sf)	CN	Description		
	4,000	98	Roofs, HSG	С	
	4,000		100.00% Im	npervious A	Area
Tc (min)	Length (feet)	Slop (ft/fl	,	Capacity (cfs)	•
6.0					Direct Entry,

#### Summary for Subcatchment 4: Subcatchment 4

Runoff = 0.04 cfs @ 12.04 hrs, Volume= 161 cf, Depth= 5.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

Area (sf)	CN Description				
383	98 Paved parking, HSG C				
383	100.00% Impervious Area				
Tc Length (min) (feet)					
6.0	Direct Entry,				

# Summary for Subcatchment 5: Subcatchment 5

Runoff = 0.11 cfs @ 12.04 hrs, Volume= 395 cf, Depth= 5.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

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Area (sf) CN Description	-
937 98 Paved parking, HSG C	
937 100.00% Impervious Area	
957 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description	
(min) (feet) (ft/ft) (ft/sec) (cfs)	
6.0 Direct Entry,	
Summary for Subcatchment 6: Subcatcl	hment 6
······································	
Runoff = 0.09 cfs @ 12.04 hrs, Volume= 338 cf, Dept	h= 5.05"
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"	hrs, dt= 0.01 hrs
Area (sf) CN Description	
803 98 Paved parking, HSG C	
803 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
6.0 Direct Entry,	
Summary for Subcatchment 7: Subcatch	nment 7
Runoff = 0.41 cfs @ 12.04 hrs, Volume= 1,464 cf, Dept	h= 5.05"
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"	hrs, dt= 0.01 hrs
Area (sf) CN Description	
3,476 98 Paved parking, HSG C	
3,476 100.00% Impervious Area	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)	
6.0 Direct Entry,	
Summary for Subcatchment 8: Subcatch	nment 8
Runoff = 0.30 cfs @ 12.04 hrs, Volume= 1,083 cf, Dept	h= 5.05"
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00	hrs, dt= 0.01 hrs

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

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Area (sf)	CN Description	
2,572	98 Paved parking, HSG C	
2,572	100.00% Impervious Area	
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)	
6.0	Direct Entry,	

# Summary for Subcatchment 9: Subcatchment 9

Runoff = 0.04 cfs @ 12.04 hrs, Volume= 139 cf, Depth= 5.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

A	rea (sf)	CN D	escription		
	331	98 Pa	aved parkir	ng, HSG C	
	331	10	00.00% Im	pervious A	Area
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•
6.0					Direct Entry,

#### Summary for Pond 1P: PR. CB-1

Inflow Area =	11,900 sf,100.00% Impervious,	Inflow Depth =	3.59"	for 10-yr event
Inflow =	0.79 cfs @ 12.04 hrs, Volume=	3,563 cf		-
Outflow =	0.79 cfs @ 12.04 hrs, Volume=	3,556 cf,	Atten=	0%, Lag= 0.1 min
Primary =	0.79 cfs @ 12.04 hrs, Volume=	3,556 cf		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 48.01' @ 12.04 hrs Surf.Area= 13 sf Storage= 13 cf

Plug-Flow detention time= 3.1 min calculated for 3,556 cf (100% of inflow) Center-of-Mass det. time= 1.7 min (764.8 - 763.1)

Volume	Invert	Avail.Storage	Storage Description
#1	47.00'	54 cf	4.00'D x 4.30'H Vertical Cone/Cylinder
Device	Routing	Invert Out	let Devices
#1	Primary	L= Inle	<b>0" Round 12" CMP</b> 22.4' CMP, end-section conforming to fill, Ke= $0.500$ t / Outlet Invert= $47.50'$ / $47.00'$ S= $0.0223$ '/' Cc= $0.900$ 0.025 Corrugated metal, Flow Area= $0.79$ sf

**Primary OutFlow** Max=0.79 cfs @ 12.04 hrs HW=48.01' TW=0.00' (Dynamic Tailwater) **1=12" CMP** (Barrel Controls 0.79 cfs @ 2.88 fps)

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# Summary for Pond 2P: PR. CB-2

Inflow Area = Inflow = Outflow = Primary =	3,476 sf,100.00% Impervious, Inflow Depth =5.05" for 10-yr event0.41 cfs @12.04 hrs, Volume=1,464 cf0.41 cfs @12.04 hrs, Volume=1,457 cf, Atten= 0%, Lag= 0.1 min0.41 cfs @12.04 hrs, Volume=1,457 cf						
Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 48.10' @ 12.04 hrs Surf.Area= 13 sf Storage= 14 cf							
Plug-Flow detention time= 7.7 min calculated for 1,457 cf (100% of inflow) Center-of-Mass det. time= 4.5 min ( 753.5 - 749.0 )							
Volume Inve	rt Avail.Storage Storage Description						
#1 47.0	0' 54 cf <b>4.00'D x 4.30'H Vertical Cone/Cylinder</b>						
Device Routing	Invert Outlet Devices						
#1 Primary	47.50' <b>12.0" Round 12" CMP</b> L= 22.4' CMP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 47.00' S= 0.0223 '/' Cc= 0.900						
	n= 0.025 Corrugated metal, Flow Area= 0.79 sf						

**Primary OutFlow** Max=0.41 cfs @ 12.04 hrs HW=48.10' TW=48.01' (Dynamic Tailwater) **1=12" CMP** (Outlet Controls 0.41 cfs @ 1.18 fps)

# Summary for Pond 3P: Permeable pavers #3

Applied discharge multiplier of 0,8 to account for horizontal infiltration area loss due to geomembrane. Some infiltration under geomembrane that may occur due to geotextile underlaying, which will allow some in-plane water movement below the membrane. Ignoring this addiitonal infiltration was ignored to be conservative as geotextile will not be selected for in-plane transmissivity.

Inflow Area = Inflow =	6,123 sf,100.0 0.09 cfs @ 12.04	0% Impervious, Inflow Depth = 0.66" for 10-yr event hrs, Volume= 338 cf					
Outflow =	0.01 cfs @ 12.00	hrs, Volume= 338 cf, Atten= 92%, Lag= 0.0 min					
Discarded = Primary =	0.01 cfs @ 12.00 0.00 cfs @ 0.00						
Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 50.48' @ 13.03 hrs Surf.Area= 803 sf Storage= 110 cf							
Plug-Flow detention time= 134.6 min calculated for 338 cf (100% of inflow) Center-of-Mass det. time= 134.6 min ( 883.6 - 749.0 )							
Volume Inv	ert Avail.Storage	Storage Description					
#1 49.8	30' 481 cf	<b>Custom Stage Data (Irregular)</b> Listed below (Recalc) 1,202 cf Overall x 40.0% Voids					

NH-Durham(NOAA) 24-hr S1 10-yr Rainfall=5.29"

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Elevati (fee	•••	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
49. 50.		0 803	0.0 103.0	0 134	0 134	0 845	
51. 51.	30	803 803	103.0 103.0	803 265	937 1,202	948 982	
Device	Routing	Inv	ert Outlet	Devices			
#1 #2	Discardeo Primary	d 49. 51.	05' <b>0.2" H</b>	in/hr Exfiltration Ioriz. Orifice/Gr d to weir flow at lo	Phase-In= 0.01'		

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**Discarded OutFlow** Max=0.01 cfs @ 12.00 hrs HW=50.31' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=49.80' TW=47.00' (Dynamic Tailwater) **2=Orifice/Grate** (Controls 0.00 cfs)

#### Summary for Pond 4P: Permeable pavers #2

Applied discharge multiplier of 0,8 to account for horizontal infiltration area loss due to geomembrane. Some infiltration under geomembrane that may occur due to geotextile underlaying, which will allow some in-plane water movement below the membrane. Ignoring this addiitonal infiltration was ignored to be conservative as geotextile will not be selected for in-plane transmissivity.

Storage area is assuming all area are sloped at 5% (1V:20H). Membrane will allow ponding of 1,0 ft in the reservoir layer.

Inflow Area =	5,320 sf,100.00% Impervious, Inflow Depth = 1.29" for 10-yr event	
Inflow =	0.50 cfs @ 12.04 hrs, Volume= 570 cf	
Outflow =	0.11 cfs @ 12.18 hrs, Volume= 570 cf, Atten= 79%, Lag= 8.7 min	
Discarded =	0.01 cfs @ 12.18 hrs, Volume= 431 cf	
Primary =	0.00 cfs @ 0.00 hrs, Volume= 0 cf	
Secondary =	0.10 cfs @ 12.18 hrs, Volume= 139 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 51.47' @ 12.18 hrs Surf.Area= 761 sf Storage= 262 cf

Plug-Flow detention time= 261.0 min calculated for 570 cf (100% of inflow) Center-of-Mass det. time= 261.0 min (1,002.5 - 741.5)

Volume	Invert	Avail.Storage	Storage Description
#1	50.00'	251 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
			626 cf Overall x 40.0% Voids
#2	50.00'	121 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
			302 cf Overall x 40.0% Voids
		371 cf	Total Available Storage

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Elevatio (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
50.0	00	0	0	0		
51.	50	580	435	435		
51.8	83	580	191	626		
Elevatio	on	Surf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
50.0	00	0	0	0		
50.	50	191	48	48		
51.	50	191	191	239		
51.8	83	191	63	302		
Device	Routing	Invert	Outlet Devices			
#1	Discarde	d 50.00'	0.500 in/hr E	Exfiltration X (	).80 over Horizontal area	Phase-In= 0.01'
#2	Seconda	γ 51.25'	0.2" Horiz. 4'	" CPP underdr	ain X 200.00 C= 0.600	
		-	Limited to weir	flow at low hea	ads	
#3	Primary	51.50'	29.0' long Sh	arp-Crested R	Rectangular Weir 2 End Co	ontraction(s)

**Discarded OutFlow** Max=0.01 cfs @ 12.18 hrs HW=51.47' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=50.00' TW=49.80' (Dynamic Tailwater) **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs)

**Secondary OutFlow** Max=0.10 cfs @ 12.18 hrs HW=51.47' TW=47.87' (Dynamic Tailwater) **2=4" CPP underdrain** (Orifice Controls 0.10 cfs @ 2.28 fps)

# Summary for Pond 5P: Permeable pavers #1

Applied discharge multiplier of 0,8 to account for horizontal infiltration area loss due to geomembrane. Some infiltration under geomembrane that may occur due to geotextile underlaying, which will allow some in-plane water movement below the membrane. Ignoring this addiitonal infiltration was ignored to be conservative as geotextile will not be selected for in-plane transmissivity.

Storage area is assuming all area are sloped at 5% (1V:20H). Membrane will allow ponding of 1,0 ft in the reservoir layer.

Inflow Area = Inflow =	4,383 sf,100.00% Impervious, 1 0.51 cfs @ 12.04 hrs, Volume=	Inflow Depth = 5.05" for 10-yr event 1,846 cf					
Outflow =	0.51 cfs @ 12.04 hrs, Volume=	1,846 cf, Atten= 0%, Lag= 0.2 min					
Discarded = Primary =	0.01 cfs @ 12.00 hrs, Volume= 0.39 cfs @ 12.04 hrs, Volume=	673 cf 175 cf					
Secondary =	0.11 cfs @ 12.04 hrs, Volume=	997 cf					
Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 52.53' @ 12.04 hrs Surf.Area= 870 sf Storage= 270 cf							

Plug-Flow detention time= 142.8 min calculated for 1,845 cf (100% of inflow) Center-of-Mass det. time= 142.9 min ( 891.9 - 749.0 )

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Volume	Invert	Avail.Stora	<u> </u>			
#1	51.00'	376		Stage Data (P erall x 40.0% \	<b>rismatic)</b> Listed below (R /oids	Recalc)
Elevatio	on Sur	f.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft) (o	ubic-feet)	(cubic-feet)		
51.0	00	0	0	0		
52.5	50	870	653	653		
52.8	83	870	287	940		
Device	Routing	Invert (	Dutlet Devices			
#1	Discarded	51.00'	0.500 in/hr Ex	cfiltration X 0	.80 over Horizontal are	ea Phase-In= 0.01'
#2	Secondary		-		ain X 200.00 C= 0.600	
	,	L	imited to weir	flow at low hea	ıds	
#3	Primary	52.50' 2	29.0' long Sha	rp-Crested R	ectangular Weir 2 End	d Contraction(s)
Discard	<b>Discarded OutFlow</b> May $= 0.01$ cfs $= 12.00$ hrs $= HW = 52.52'$ (Free Discharge)					

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**Discarded OutFlow** Max=0.01 cfs @ 12.00 hrs HW=52.52' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.01 cfs)

**Primary OutFlow** Max=0.39 cfs @ 12.04 hrs HW=52.53' TW=51.08' (Dynamic Tailwater) **3=Sharp-Crested Rectangular Weir** (Weir Controls 0.39 cfs @ 0.53 fps)

**Secondary OutFlow** Max=0.11 cfs @ 12.04 hrs HW=52.53' TW=48.01' (Dynamic Tailwater) **2=4" CPP underdrain** (Orifice Controls 0.11 cfs @ 2.53 fps)

#### Summary for Pond E1: EX. CB-2310

Inflow Area =	2,903 sf,100.00% Impervious,	Inflow Depth =	5.03" for 10-yr event
Inflow =	0.34 cfs @ 12.04 hrs, Volume=	1,216 cf	
Outflow =	0.34 cfs @ 12.04 hrs, Volume=	1,210 cf,	Atten= 0%, Lag= 0.1 min
Primary =	0.34 cfs @ 12.04 hrs, Volume=	1,210 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 47.82' @ 12.04 hrs Surf.Area= 13 sf Storage= 10 cf

Plug-Flow detention time= 8.0 min calculated for 1,210 cf (99% of inflow) Center-of-Mass det. time= 4.3 min (758.3 - 754.0)

Volume	Invert	Avail.Storage	e Storage Description
#1	47.00'	54 c	f 4.00'D x 4.30'H Vertical Cone/Cylinder
Device	Routing	Invert O	utlet Devices
#1	Primary	L= In	<b>2.0" Round 12" CMP</b> = 22.4' CMP, end-section conforming to fill, Ke= 0.500 let / Outlet Invert= 47.50' / 47.00' S= 0.0223 '/' Cc= 0.900 = 0.025 Corrugated metal, Flow Area= 0.79 sf
Driman		May-0 34 cfs @	12.04 hrs $HW = 47.82'$ $TW = 0.00'$ (Dynamic Tailwater)

**Primary OutFlow** Max=0.34 cfs @ 12.04 hrs HW=47.82' TW=0.00' (Dynamic Tailwater) **1=12" CMP** (Barrel Controls 0.34 cfs @ 2.31 fps)

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#### Summary for Pond E2: EX. CB-2293

Inflow Area =	2,572 sf,100.00% Impervious,	Inflow Depth =	5.05" for 2	10-yr event
Inflow =	0.30 cfs @ 12.04 hrs, Volume=	1,083 cf		
Outflow =	0.30 cfs @ 12.04 hrs, Volume=	1,077 cf,	Atten= 0%,	Lag= 0.1 min
Primary =	0.30 cfs @ 12.04 hrs, Volume=	1,077 cf		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 47.96' @ 12.04 hrs Surf.Area= 13 sf Storage= 12 cf

Plug-Flow detention time= 9.8 min calculated for 1,077 cf (99% of inflow) Center-of-Mass det. time= 5.7 min (754.7 - 749.0)

Volume	Invert	Avail.Storage	Storage Description
#1	47.00'	54 cf	4.00'D x 4.30'H Vertical Cone/Cylinder
Device #1	Routing Primary		et Devices D" Round 12" CMP
π1	T TIMOT Y	L= 2 Inle	22.4' CMP, end-section conforming to fill, Ke= 0.500 t / Outlet Invert= $47.50'$ / $47.00'$ S= 0.0223 '/' Cc= 0.900 0.025 Corrugated metal, Flow Area= 0.79 sf

**Primary OutFlow** Max=0.30 cfs @ 12.04 hrs HW=47.95' TW=47.82' (Dynamic Tailwater) **1=12" CMP** (Outlet Controls 0.30 cfs @ 1.27 fps)

#### Summary for Pond E3: CB 2078

[57] Hint: Peaked at 50.61' (Flood elevation advised)

Inflow Area =	13,022 sf, 70.32% Impervious,	Inflow Depth =	4.32" for 10-yr event
Inflow =	1.34 cfs @ 12.04 hrs, Volume=	4,692 cf	
Outflow =	1.34 cfs @ 12.04 hrs, Volume=	4,692 cf,	Atten= 0%, Lag= 0.0 min
Primary =	1.34 cfs @ 12.04 hrs, Volume=	4,692 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 50.61' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	50.00'	<b>12.0"</b> Round Outlet L= 90.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 50.00' / 49.10' S= 0.0100 '/' Cc= 0.900
			n= 0.012 Concrete pipe, finished, Flow Area= 0.79 sf

**Primary OutFlow** Max=1.33 cfs @ 12.04 hrs HW=50.61' TW=0.00' (Dynamic Tailwater) **1=Outlet** (Inlet Controls 1.33 cfs @ 2.66 fps)

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# Summary for Link PA-1: POA-1

Inflow Area =		15,521 sf,	65.30% Im	pervious,	Inflow Depth =	4.20"	for	10-yr event
Inflow	=	1.56 cfs @ 12	2.04 hrs, V	olume=	5,433 cf			
Primary	=	1.56 cfs @ 12	2.04 hrs, V	/olume=	5,433 cf,	Atten=	0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

# **Summary for Link PA-2: POA-2**

Inflow Area =	14,803 sf,100.00% Impervious,	Inflow Depth =	3.86"	for 10-yr event
Inflow =	1.13 cfs @ 12.04 hrs, Volume=	4,766 cf		
Primary =	1.13 cfs @ 12.04 hrs, Volume=	4,766 cf,	Atten=	0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

3. PLANS

